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# ADAPTIVE REFINEMENT CRITERION FOR ELLIPTIC PROBLEMS DISCRETIZED BY FEM

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#### SUMMARY

In a recent paper<sup>1</sup> we presented a data structure to be used with multigrid techniques on nonhomogeneously refined FEM meshes. This paper focuses on the adaptive refinement techniques used there. The error estimate is obtained from standard Taylor series. For each element we compute its efficiency in terms of the size, the norm of the second derivatives of the unknown and the parameter p, where  $L_p$  is the chosen norm. The way the norm influences the optimal mesh is studied. The number of elements to be refined at each step is such to produce a fast convergence to the optimal mesh, followed by successive homogeneous refinements. We hope that the analysis of these two subjects could be of value for people working with other (perhaps very dissimilar) adaptive refinement techniques (error estimate and data structure, for instance).

#### 1. INTRODUCTION

In previous years, more efficient solutions of discretized continuum problems were searched in two ways: optimal meshing and more efficient solution of the resulting discrete equations. In our work optimal finite-element meshing is achieved through a process of adaptive refinement, and the solution is obtained at each step with an extension of the multigrid method for non-structured meshes. This subject has been dealt with in depth in a recent paper.<sup>1</sup>

With reference to the adaptive refinement strategy, much effort was devoted to two of the most important topics in this area, i.e. the error estimator and the type of adaptive improvement for use. To begin with the error estimator, we could make a brief list of the various kinds of estimators that exist in the literature. These are based on:

- (a) resolution of local problems. The estimators within this class produce the estimates of local errors over individual elements or over a patch of elements surrounding each of the elements by defining an indicator of how much the approximation fails to satisfy the governing differential equations and boundary conditions<sup>2-5</sup>
- (b) interpolations methods and superconvergence. These methods use the interpolation theory of finite elements in Sobolev norms to produce the estimates of the local errors over individual elements<sup>6-10</sup>
- (c) complementary variational principle. These ones, valid for self-adjoint elliptic problems, use the duality theory of convex optimization to derive upper and lower bounds of the element errors<sup>11</sup>

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- (d) estimates of derivatives by incremental quotients of  $u_h^{12}$
- (e) residual error estimates. The value of the residual over each element is taken as a measure of the error size and is used as a refinement criterion.<sup>13-17</sup>

For our work we adopt an estimator that falls inside item (b). Our algorithm uses an error indicator based on the truncation error obtained by Taylor series expansions. It has several attractive features, as follows:

- (1) The interpolation error is a local quantity defined for individual elements. Any local changes in mesh affect the values of the interpolation error on the elements where the changes have been made.
- (2) It is very easy to implement in a finite-element code, and has low computational cost.
- (3) In relation to our applications, the fact that the error indicators would be sensible to the high first derivative of the solutions is a good feature because the problems to be solved have this type of discontinuity.

On the other hand, extensions to non-elliptic problems do not produce the same results. The error indicator and element size serve to compute a parameter that plays the role of an element computational efficiency. This point will be dealt with in depth in Section 2.

Continuing with the other topics, we come to discuss the refinement type to be used. There are four principal types:

- (a) *h*-type versions
- (b) *p*-type versions
- (c) h-p type versions
- (d) node relocation or *R*-type.

In the first strategy, the order of polynomials used to interpolate the solution is kept constant but the mesh size varies. In the second strategy the order of polynomial approximation inside the element is variable and the element size fixed. The third strategy is based on a mixture of the two strategies above. In the fourth strategy, the location of the nodes is changed to improve the finite-element solution, keeping the number of nodes and the degree of the elements fixed.

We do not make any specific reference to the great number of papers published on this topic, but we just mention one state-of-the-art paper, <sup>18</sup> in which almost 200 references can be found. It is a common problem of all types of strategies to find an optimal mesh. Our work is based on the *h*-type strategy as part of a full multigrid method.

In our work, we define an optimal mesh as the mesh, among the class of admissible ones, for which the efficiency for all the elements should be constant and should give a minimum error for a fixed computational effort. The strategy to choose the amount of elements for refinement is discussed later on.

We decide to use h-type refinement over a mesh composed of quadrangular elements. The data structure used is similar to those appearing in References 19 and 20, with some particular aspects due to its application in a multigrid context.<sup>1</sup>

# 2. THE ERROR ESTIMATOR

We estimate the error as being given mainly by the interpolation one

$$||u^{R} - u|| \leq ||u^{R} - u^{I}|| + ||u^{I} - u|| \approx ||u^{I} - u||$$
(1)

This assertion is true in  $L_2$  norms. Sewell used it as valid in the  $L_{\infty}$  context, and in this paper

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we use it in general  $L_p$  norms. Like Sewell, we have no theoretical foundations to do this. The  $L_p$ -norm error is calculated element by element and the local error is approximated by a truncated Taylor series:<sup>21</sup>

$$\| u^{I} - u \|_{p} = \left( \int_{\Omega} | u^{I} - u |^{p} d\Omega \right)^{1/p} = \left( \sum_{e} \int_{\Omega_{e}} | u^{I} - u |^{p} d\Omega \right)^{1/p}$$
$$| u^{I}(\mathbf{x}) - u(\mathbf{x}) | \approx \left| \sum_{i,j=1}^{n_{d}} \left( \frac{\partial^{2} u}{\partial x_{i} \partial x_{j}} \right)_{v_{k}} \Delta x_{i} \Delta x_{j} \right|$$
(2)

we take  $v_k$  as the nearest node of the element containing the point x, so that:

$$\Delta x_i \leqslant \frac{h_e}{2} \tag{3}$$

$$\left|\sum_{i,j=1}^{n_d} \left(\frac{\partial^2 u}{\partial x_i \ \partial x_j}\right)_{v_k} \Delta x_i \ \Delta x_j\right| \leq \sum_{i,j=1}^{n_d} \left|\left(\frac{\partial^2 u}{\partial x_i \ \partial x_j}\right)_{v_k} \Delta x_i \ \Delta x_j\right|$$
$$\leq \sum_{i,j=1}^{n_d} \left|\left(\frac{\partial^2 u}{\partial x_i \ \partial x_j}\right)_{v_k}\right| \frac{h^2}{4} \leq \tilde{\Phi}_e \frac{h^2}{4} \tag{4}$$

where

$$\tilde{\Phi}_{e} = \max_{v_{k} \in \Omega_{e}} \left\{ \sum_{i,j=1}^{n_{e}} \left| \left( \frac{\partial^{2} u}{\partial x_{i} \partial x_{j}} \right)_{v_{k}} \right| \right\}$$
(5)

Replacing (4) in (2) we obtain our error estimator:

$$|| u^{R} - u ||_{p} \approx \left( \sum_{e} \Phi_{e}^{p} \left( \frac{h_{e}}{2} \right)^{2p} \Omega_{e} \right)^{1/p} = E_{p}$$
(6)

where  $\Phi_e$  is calculated with an expression similar to (5), replacing the derivatives of the exact solution u by

$$\left(\frac{\partial^2 u}{\partial x_i \ \partial x_j}\right)_{\nu_k} \approx \left(-\int_{\Omega} \frac{\partial N_k}{\partial x_i} \frac{\partial u^R}{\partial x_j} \,\mathrm{d}\Omega\right) / \left(\int_{\Omega_B} N_k \,\mathrm{d}\Omega\right) \tag{7}$$

Usually, one of the most important requirements to the error estimator is to detect singularities. Since our estimate is based on the second derivatives, it is evident that it will detect jump singularities (as shocks in compressible fluid dynamics), phase change and general free boundary problems, domain irregularities (as corners in fluid dynamics, elasticity, etc...), boundary data discontinuities, etc.... Even in the case where the second derivative does not exist the error estimator will get very high values in such a situation. Hence, the use of the estimator as a driving force to the feedback procedure is guaranteed.

Now we are going to discuss the use of our estimator as a stopping criterion. Starting with the definition (6) and supposing that  $\Phi_{\min} > 0$  is the lower bound for the  $\Phi_{es}$ ,

$$\left(\frac{4E_p}{\Phi_{\min}}\right)^p \ge \sum_e h_e^{2p} \Omega_e \ge h_{\min}^{2p} \sum_e \Omega_e = h_{\min}^{2p} \Omega$$
(8)

which implies that

$$h_{\min} \leq \left(\frac{4E_p}{\Phi_{\min}}\right)^{1/2} \frac{1}{\Omega^{1/2p}} \leq C_p E_p^{1/2}$$
 (9)

so that, if  $E_p \to 0$ , then  $h_{\min} \to 0$  and (if convergence is verified)  $u^R \to u$ .

#### 3. REFINEMENT STRATEGY

In general, a refinement strategy will give us a set of element parameters  $\{\eta_e\}_{e=1}^{N_e}$  so that one refines those elements in which  $\eta_e$  exceeds a certain threshold value. If the refinement criterion is, for instance, to reduce the local error, one can define

$$\eta_e = \Phi_e h_e^2 \approx \max_{\mathbf{x} \in \Omega_e} |u(\mathbf{x}) - u^R(\mathbf{x})|$$
(10)

Another criterion could be to reduce the  $L_p$ -norm of the error over the element:

$$\eta_{e} = \Phi_{e} h_{e}^{2+n_{d}/p} \approx 4 \left( \int_{\Omega_{e}} |u - u^{R}|^{p} d\Omega \right)^{1/p} = 4 ||(u - u^{R})|_{\Omega_{e}} ||_{p}$$
(11)

One can generalize all these criteria as  $\eta_e = \Phi_e h_e^m$ , with  $0 < m < \infty$ . A small *m* will give a refinement extremely sensitive to variations in the second derivatives; the opposite is true for the case of a large *m*, so we will try to find the appropriate value of *m*. This will be done by optimization of the element error reduction penalized with the increase in computational work that takes place during the refinement of the particular element.<sup>22</sup>

The computational work is given by

$$W \approx wN_e = w \sum_e 1 \approx w \sum_e h^{-n_d} \Omega_e \approx w \int_{\Omega} h^{-n_d} d\Omega = W[h(\mathbf{x})]$$
(12)

where h is taken as a continuous function. The error can be written also as a functional of h as:

$$E[h(\mathbf{x})] = \frac{1}{4} \left( \int_{\Omega} \tilde{\Phi}^{p}(\mathbf{x}) h^{2p}(\mathbf{x}) \, \mathrm{d}\Omega \right)^{1/p}$$
(13)

(Note that  $\Phi(\mathbf{x})$  has been replaced by  $\tilde{\Phi}(\mathbf{x})$ ). We introduce the computational work in the functional via a Lagrange multiplier  $\lambda$  and pose the Euler equations to find the extrema

$$\delta(E[h(\mathbf{x})] + \lambda W[h(\mathbf{x})]) = 0 \tag{14}$$

which implies

$$\frac{1}{p} E^{1-p} \Phi^{p} 2^{p} \left(\frac{h}{2}\right)^{2p-1} \frac{1}{2} + \lambda w(-n_{d}) h^{-n_{d}-1} = 0$$
(15)

so that

$$\eta_e = \Phi_e h_e^{2 + n_d/p} = \left(\frac{\lambda w n_d 2^{2p-1}}{E^{1-p}}\right)^{1/p} = \text{cte}$$
(16)

which is the same as the second definition described at the beginning of this section; hence the optimal criterion is to reduce the  $L_p$ -norm of the error over the element.  $\eta_e$  can be considered as the inverse of an efficiency:

$$\eta_e^p \propto \lambda = \frac{-\delta E}{\delta W} \tag{17}$$

For the elements with a large  $\eta_e$ , a strong reduction  $-\delta E$  of the error can be obtained through a little computational work  $\delta W$ , and the converse is true for small  $\eta_e$ .

The elements to be refined at each refinement step are those which have a low efficiency, i.e. those which satisfy

$$\eta_e > \beta \eta_{\max} \tag{18}$$

where  $\eta_{\text{max}}$  is the maximum value of  $\eta_e$  over all the elements and  $0 < \beta < 1$ .

### 4. THE NUMBER OF ELEMENTS TO BE REFINED

We will discuss now the choice of  $\beta$  or, in other words, the number of elements that must be refined at each refinement step. As mentioned above, the optimal mesh will be that one with a constant  $\eta_e$ . It implies an optimal mesh size  $h_{opt} \propto \tilde{\Phi}^{-1/m}$ . Note that the optimal mesh is defined modulo a homogeneous refinement. A value of  $\beta$  close to 1 will produce a very slow convergence to the optimal mesh because only very few elements are refined at each step. Conversely, if  $\beta$  is close to 0 nearly all the elements are refined at each step and the process will not converge at all to the optimal mesh. The optimal  $\beta$  will be that which gives a fast convergence to a mesh with a narrow gap of  $\eta_s$ .

To find the optimal  $\beta$  we will make a simplified analysis based on the following model. Once an element with  $\eta_e = \Phi_e h_e^m$  is refined,  $2^{n_d}$  sons are created, with

$$\eta_e' = \Phi_e \left(\frac{h}{2}\right)^m = \eta_e 2^{-m} \tag{19}$$

and the other elements remain with their respective  $\eta_e$  unchanged.

It implicitly assumes that the  $\Phi_e s$  do not change very much when the elements are refined, which is likely to be so, due to the convergence of  $u^R$  to u. Let us now consider the  $2^{-m} \leq \beta < 1$  case (see Figure 1), each curve represents the distribution of elements over  $\eta$  for the  $G^R$ -mesh (the mesh obtained after R refinement steps), so that the area below the curve in any interval  $[\eta_a, \eta_b]$  is representative of the number of elements which have  $\eta_a \leq \eta_e \leq \eta_b$  (note: the  $\eta$  axis is logarithmic).

In the former steps ( $R < R_C$ ; the expression for  $R_C$  is shown later), the elements in the interval  $[\beta \eta_{\max}^{R-1}, \eta_{\max}^{R-1}]$  (the shadowed area in Figure 1(a)) are moved left a distance  $\Delta = m \log 2$  to their position in the shadowed area of Figure 1(b). The net area added below the curve is  $(2^{n_d} - 1)$  times the shadowed area in Figure 1(a). Note that  $\eta_{\max}$  is moved left a distance  $S = -\log \beta$  and  $\eta_{\min}$  remains unchanged. This is so in the subsequent refinement steps until at a certain step  $R_C$  ( $G^{R_C-1} \rightarrow G^{R_C}$ ):

$$\eta_{\min}^{R_{\rm C}} = 2^{-m} \beta \eta_{\max}^{R_{\rm C}-1} = 2^{-m} \beta^{R_{\rm C}} \eta_{\max}^{0} \leqslant \eta_{\min}^{0}$$
(20)

is satisfied, so that

$$R_{\rm C} = \left[\frac{1}{S} \log\left(\frac{\eta_{\rm max}^0}{2^m \eta_{\rm min}^0}\right)\right] \tag{21}$$

where [] denotes the integer part of its argument. In the  $R_c$  step the  $\eta_{\min}$  value does not remain constant, and for  $R > R_c$  the situation is like that described in Figures 1(c, d): the elements in the interval  $[\beta \eta_{\max}^{R-1}, \eta_{\max}^{R}]$  are moved into the interval  $[2^{-m}\beta \eta_{\max}^{R-1}, 2^{-m}\eta_{\max}^{R}]$  exactly to the left of the interval whose elements remain fixed.

As a consequence, we have for  $R > R_C$ :

• a constant gap: 
$$\Delta = \log\left(\frac{\eta_{\max}^{K}}{\eta_{\min}^{R}}\right) = m \log 2$$

• a constant shift: 
$$S = -\log\left(\frac{\eta_{\max}^{R-1}}{\eta_{\max}^{R}}\right) = -\log\left(\frac{\eta_{\min}^{R+1}}{\eta_{\min}^{R}}\right) = -\log \beta$$

We can see that, from all the  $\beta$ s with  $2^{-m} \leq \beta < 1$ , the value  $\beta_{opt} = 2^{-m}$  is the best one because:

• the shift is the highest:  $S = m \log 2$ 



Figure 1. The  $2^{-m} \leq \beta < 1$  case,  $S = -\log \beta$ ,  $\Delta = m \log 2$ 



Figure 2. The  $0 < \beta \leq 2^{-m}$  case,  $S = m \log 2$ ,  $\Delta = -\log \beta$ 

- the number of steps  $R_{\rm C}$  to attain the best mesh is the lowest (see (21))
- the gap is the same as for all the other  $\beta$ s within the interval.

In the same way, it can be shown that for the  $0 < \beta \leq 2^{-m}$  case we have (see Figure 2):

- a shift  $S = m \log 2$
- a gap  $\Delta = -\log \beta$  for  $R \ge R_c$ , where  $R_c$  is given by the same expression (21).

We have in this interval:

- the shift is the same for all  $\beta$ s
- the number of steps  $R_c$  to attain the optimal mesh is the same for all  $\beta$ s
- the gap is the narrowest for  $\beta = \beta_{opt}$ .

So the choice  $\beta = \beta_{opt}$  is optimal over all  $0 < \beta < 1$ .

We have studied this point in detail because we think that it can be applied to other error estimators, as long as the model described above holds. At each circumstance the corresponding m value must be found by a theoretical error analysis or by a heuristic one.

## 5. NUMERICAL EXAMPLES

We solve the Laplace equation in the unit square with Dirichlet conditions:

$$\begin{cases} \Delta u = 0 & \text{in } \Omega = [0, 1] \times [0, 1] \\ u = \bar{u} & \text{in } \partial \Omega \end{cases}$$
(22)

where:

$$\bar{u} = ((x+\varepsilon)^2 + y^2)^{\alpha/2} \cos\left(\alpha \tan^{-1}\left(\frac{y}{x+\varepsilon}\right)\right) = \Re\{f(z)\}$$

$$z = x + iy, \quad i = \sqrt{-1}$$

$$f(z) = (z+\varepsilon)^{\alpha}, \quad \alpha, \varepsilon \in \mathbb{R}$$
(23)

f is (depending on the choice of  $\alpha$ ) singular on  $z = -\varepsilon$ . Hence, by varying  $\alpha$  and  $\varepsilon$ , we control the irregularity of u (over  $\Omega$ ). In fact u is the analytical solution for potential flow around a re-entrant corner (see Figure 3). For  $\alpha = -1$  the flow corresponds to that of a dipole. The norm of the derivatives is easily calculated as follows:

$$|\nabla u| = \left|\frac{\mathrm{d}f}{\mathrm{d}z}\right| = \alpha r^{\alpha - 1}$$

$$|\nabla \nabla u| = \sqrt{\left\{\left(\frac{\partial^2 u}{\partial x^2}\right)^2 + \left(\frac{\partial^2 u}{\partial y^2}\right)^2 + 2\left(\frac{\partial^2 u}{\partial x \partial y}\right)^2\right\}}$$

$$= \sqrt{2} \left|\frac{\mathrm{d}^2 f}{\mathrm{d}z^2}\right| = \sqrt{2} |\alpha(\alpha - 1)| r^{\alpha - 2}$$
(24)

So, using standard inequalities relating different p-norms on finite-dimension spaces,

$$\bar{\Phi} = \mathcal{C}(x, y) \left| \alpha(\alpha - 1) \right| r^{\alpha - 2}$$

with  $\sqrt{2}/3 \leq C(x, y) \leq \sqrt{2}$ .



Figure 3. Test problem



Figure 4. Mesh convergence: (a)-(d) initial meshes; (e) final mesh for mesh (a); (f) final mesh for meshes (b)-(d)

## 5.1. Mesh convergence

The first example deals with the mesh convergence of the refinement process, i.e. we expect that, starting with different initial meshes  $G^0$ , we will get similar meshes after several refinement steps.

We have set  $\alpha = 0.1$  and  $\varepsilon = 10^{-3}$  and we have taken as initial meshes those indicated in Figures 4(a-d)). The corresponding final meshes are: 4(e) for 4(a) and 4(f) for 4(b-d). The Figures show a satisfactory convergence to the optimal mesh, regardless of the initial mesh chosen by the user. The final meshes shown are obtained after seven refinement steps for the (a-c) cases and after five steps in the (d) case, which is obviously the best initialization. However, the CPU times are almost the same because the most expensive steps are the final ones, where the mesh configuration is the same.

#### 5.2. $\beta$ choice

The problem parameters are:  $\alpha = 0.5$ ,  $\varepsilon = 10^{-12}$  and p = 0.25. In Figure 5(a) we have the initial distribution curve of  $\eta_{es}$ . The interval shown is always  $[\log \eta_{max}^{R} - 4, \log \eta_{max}^{R}]$ . We have



Figure 5. Choice of  $\beta$  parameter

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run this problem with:

- (i)  $\beta = \beta_{opt} = 2^{-10} \approx 0.001$ . After three refinement steps we obtain the curve shown in Figure 5(b) with a gap  $\Delta \approx 2$  (neglecting the tails of the curve to the right and to the left of the main peak)
- (ii)  $\beta = 0.1 \gg \beta_{opt}$ . We show the curves for R = 3 (Figure 5(c)) and R = 7 (Figure 5(d)). Note that the gap is in both curves  $\Delta \approx 3$ . This high value for  $\Delta$  is expected since we are in the case  $\beta > \beta_{opt}$  and then we would need a great number of additional steps to reach the optimal mesh.

### 5.3. Choice of m and p parameters

It was shown in Section 5 that the optimal choice of m for a given norm  $L_p$  is m = 2 + 2/p (in 2D). It means that if we plot the *p*-norm of the error  $|| u^{\mathbb{R}} - u ||_p$  against the CPU time for several *m*-values we should find that the choice m = 2 + 2/p gives the fastest reduction of the error. To make this clear we will show a numerical example in which we have made nine runs with all the combinations  $(m_i, p_j)$  with:

$$m_1 = 2 \cdot 2, \qquad m_2 = 4, \qquad m_3 = 22$$
  
 $n_1 = 10, \qquad n_2 = 1, \qquad n_3 = 0 \cdot 1$ 

In Figures 6(a-c) we see the  $L_p$ -norm of the error with the three refinement criteria  $m_1$ ,  $m_2$  and  $m_3$ . The expected behaviour is found for  $p_1$  and  $p_2$ . For  $p_3$  (Figure 6(c))  $m_2$  was the optimum; however  $m_3$  was close to it and the runs should be extended to reach a final conclusion. In



Figure 6. Choice of *m* and *p*: (a)  $p_1 = 10$ ; (b)  $p_2 = 1$ ; (c)  $p_3 = 0.1$ 



Figure 6. (Continued)

practice one is interested in norms  $L_1$  and  $L_2$ . This gives *m*-values 4 and 3, respectively. Note that m = 4 was nearly optimal in all the norms  $p_i = 0.1$ , 1 and 10, so that we recommend, in general, a choice of *m* near these values.

# 6. CONCLUSIONS

This study is concerned with the already popular adaptive refinement technique and highlights some important points about an optimal use of it. An estimator based on interpolation theory is used and the numerical results give evidence that its behaviour in the presence of different types of discontinuities is correct. A good way to choose the amount of elements to be refined in each step, based on the optimization of a computational efficiency, is developed. Several examples have shown an acceptable accord between the theoretical aspects and the practical ones. Here we include only the Laplacian problem. Probably, future works in this direction would lead to a better utilization of the computational resources.

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### **APPENDIX**

## Nomenclature

# e = element index

- $G_l^R = R$ -step mesh 'unrefined' to level l
- h = element size
- $L_p = norm$
- l = level number
- m = exponent defining the parameters of  $\eta$
- $n_{\rm d}$  = number of spatial dimensions
- R = refinement step index:  $G^{R-1} \rightarrow G^R$  during step R
- S =logarithmic shift at each refinement step
- u = scalar valued functions over  $\Omega$
- w = average resolution work by element
- $\beta$  = parameter defining the  $\eta$  threshold value for refinement;  $\beta_{opt}$  = optimal value
- $\gamma = maximum$  level
- $\delta$  = first variation of a functional.
- $\Delta$  = logarithmic gap, i.e. the width of the distribution curve in logarithmic scale
- $\varepsilon =$  shift from the corner in the numerical examples
- $\eta$  = element refinement parameters; one refines the elements with high  $\eta$ ;  $\eta_{max}$ ,  $\eta_{min}$  are the extreme values
- $\Omega =$ domain.

Super| subscripts

(sub)	e = element index
(supra)	I = finite-element interpolation
(sub)	l = level of 'unrefinement'
(sub/supra)	p = parameter in the norm definition
(supra)	R = level of refinement.

#### Special symbols

 $\mathbf{x} =$ vectors in bold

||x|| = norm of a vector

 $()_x = evaluate () at x$ 

[x] = the integer part of x

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