Measurement of Moisture Content and Volume Change Distribution Inside Cement Paste Specimens Using X-Ray CT Imaging

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Abstract. The purpose of this study was to clarify the internal change of concrete structures during drying. Therefore, we used X-ray CT to investigate water content and volume changes inside cement paste specimens during drying. Changes in the CT image intensities and measurements on the images indicated water content and volume changes, including local changes detected with digital volume correlation. Next steps will be to understand the link between volume changes and the local water content.

Keywords: Cement Past, Drying Shrinkage, Moisture Content, X-Ray CT, Digital Volume Correlation.

1 Introduction

Concrete contains a lot of free water. When free water evaporates by drying, volume changes can occur. Such volume changes due to drying can cause cracks on the surface of concrete structures, resulting in a decreased durability of the structure.

The estimation of volume changes in concrete have usually been calculated based on the length change of a specimen (JIS A 1129-3). However, it is not only the shrinkage of cement paste that should be considered, but also shrinkage and distribution of aggregates also influence volume changes in concrete, for example Zhanga, W. *et al* (2013) and Alexander, MG. (1996). Furthermore, as moisture is transferred from the surface, the moisture content is different between the surface and the interior. For these reasons, it is difficult to estimate the complicated volume change only by the apparent externally measured size change of a specimen.

For the above reasons, we considered that a method that can measure the moisture content and volume change inside concrete in three dimensions (3D) is necessary. Previously, Sant, G. and Weiss, J. (2009). and Hong, S., *et al* (2019) used an X-ray CT apparatus to mesurement changing of water content and cracking inside the specimen. T. Fumoto also developed an Xray CT system to estimate moisture content and composition of concrete after high temperature heating and to measure 3D volumetric strain fields in concrete under loading stress, for example Fumoto, T. and Hall, S (2019) and Fumoto, T., Mizuno, S. and Ozawa, M. (2016). Here we extend this previous work to examine the moisture content and volume change inside specimens during drying.

In this study we performed a length-change test on a cylindrical specimen of cement paste, which is a basic approach for measuring drying shrinkage, but we study the distribution of volume changes inside the sample using X ray CT and make image measurements at different

stages of the drying.

2 Experiment Methods

2.1 Specimen

To maximise the possibility of being able to make 3D measurements of the internal specimen changes during drying, a paste specimen that would give a large volume change was prepared. In addition, to study the effect of aggregates (crushed stone, in this case) on the internal deformation, paste specimens were prepared with a particle of crushed stone or crushed brick placed in the centre. Only a single particle was included to be able to visualize the effects around the aggregate without the influence of adjacent particles.

Table 1 shows the mixture proportions of the paste used in this study. In addition to ordinary Portland cement, zirconia balls with a particle size of 0.3 mm (density $6.07 \text{ g}/\text{cm}^3$) were mixed into the paste (the samples had 0.75% of the paste volume as zirconia balls) to provide more enhanced intensity patterns in the tomography images for improving the accuracy of the image measurements.

Table 1. Mixture proportions of paste.					
W/C	Unit content (kg/m ³)				
(%)	Water	Cement	Thickener agent	Thickener agent	Zirconia ball
60	652	1088	32.6	0.326	45.4

5 L of paste was mixed in a planetary mixer, from which three specimens were made. Figure 1 shows an image of one of the specimens and the coordinate system used. The dimensions of the specimens were 75 mm in diameter and 144 mm in height. When placing the paste into the moulds, bolts with a diameter of 6 mm and a length of 35 mm were attached to the upper and lower surfaces of the specimen. For two specimen, crushed stones (surface dry density 2.63g / cm^3 , water absorption 1.6%, particle size about 30mm) and crushed bricks were placed in the centre in a saturated surface - dry condition.

The samples were demoulded the next day and, immediately after, an epoxy resin was applied to the upper and lower surfaces of the specimen so that moisture could escape only from the sides. In addition, a PVC pipe embedded with 12 ceramic balls (diameter 5 mm) was attached to each specimen to reduce mechanical errors and enabling an affine transformation to align images, following Ura, T., Fumoto, T and Takehara, K. (2016). The PVC pipe had 32 holes, with a diameter of 1 cm, arranged from the vertical-centre to the bottom to not prevent moisture dissipation. The specimens were stored in a constant temperature and humidity chamber at a 20 ± 1 ° C and a humidity of $60 \pm 5\%$.

2.2 Measurement Method

Length change measurements and X-ray CT scans were performed after drying periods of 0, 5, 8, 13, 21, 35 and 134 days. Shrinkage strain was measured according to the measurement method of JIS A 1129-3. The X-ray CT imaging was performed using an apparatus that were shows in Fumoto, T. (2013) in detail. For each CT measurements, the center height of the specimen \pm 35mm was scanned using the imaging parameters shown in Table 2 and with a

cubic image voxels with a side length of 0.123 mm. 3D deformation measurements inside the specimens were made using digital volume correlation (DVC) with the software *TomoWarp2* of Tudisco et al.(2017). For the DVC measurements, the correlation window for the correlation calculation was a cube of about 3 mm side length and the distance between correlation windows (the node spacing) was about 1.5 mm.



Figure 1. Design and photo of the specimen.

From the measurement results, the apparent length change of the specimen and the internal volumetric strain distribution were calculated. The apparent length change was calculated from the average value of the DVC-derived z-displacement in two cross-sections positioned at \pm 20 mm from the centre in the z-direction and dividing the difference between these values by 40 mm. DVC strains were determined from the difference of displacement between adjacent subsets and the local volume strain was calculated by,

$$\varepsilon_{\rm vol} = \varepsilon_{\rm x} + \varepsilon_{\rm y} + \varepsilon_{\rm z} \tag{1}$$

where ε_x , ε_y and ε_z are the normal strains in each direction.

In the X-ray CT images, the intensity indicating the relative value of X-ray absorption is affected by the density and composition. Since the apparent density decreases due to drying from the side of the specimen, the apparent density reduction may be indicated as a decrease in the intensity of the X-ray CT image. Therefore, the moisture content variations were estimated using the intensity distribution in the radial direction over a series of concentric virtual cylinders, centred on the axis of the sample, of 2.5 mm thickness and spanning a height of \pm 25 mm from the z-direction centre of the specimen in the X-ray CT images. The average value of the intensity distribution was calculated over each cylinder, and the transition of the average intensity from the surface to the inside of the specimen was calculated.

3 Experimental Results and Discussion

3.1 Shrinkage Strain

Figure 2 shows the shrinkage strain as a function of time obtained from the length change measurements. In the case of the paste, shrinkage strain began to increase from the start of drying and increased linearly until the drying period of 35 days, reaching about 3200×10^{-6} . After that, the shrinkage strain increased to about 6000×10^{-6} after 134 days of drying and appear to have reach a steady state. The length change for the crushed stone and crushed brick samples was smaller than that of the paste by about 500×10^{-6} at 35 days and about 300×10^{-6} at 134 days of drying. This is considered to result from the reduced paste volume due to the presence of the stone/brick particles.



The apparent length change calculated from the DVC calculation has been included in Figure 2. For the paste, the DVC calculated value was larger than length change value until 35 days of drying period, but it converged to the the same value by the end. On the other hand, for the crushed stone, the DVC calculated length change was about 1000×10^{-6} smaller, and for the crushed brick it was about 1700×10^{-6} smaller. These tendencies are attributed to the fact that the DVC-based calculation of the length change considered the z-direction displacement over the entire cross section of the specimen and, thus, included changes in the drying condition from the surface as well as expansion due to cracks.

3.2 Observation of X-Ray CT Images

Figure 3 shows XZ cross-section images for each drying time the three samples. For the paste sample, the image intensity is seen to decreased as the drying period increases and the specimen has only a small crack after 35 days of drying. However, for the samples containing a particle, cracks can be seen at early drying stages, which became longer and wider as the drying progresses. Some of the cracks appear to have occurred at positions where there is an abrupt change in the particle surface angle. These cracks are thought to have formed due to constraints through adhesion at the particle surface.

Figure 4 shows the intensity change as a function of position from sample surface for the paste specimen. The intensity can be seen to have decreased near the surface at 5 - 8 days of drying. After about 8 days, the intensity changed significantly near the centre. After 134 days

of drying, the intensity reached almost the same value at the centre as at the surface. As shown in Figure 2, it is expected that the water movement had reached an equilibrium by this time.

Figure 5 shows the intensity rate based on intensity difference between saturation and equilibrium, which can be regarded as the rate of water reduction until reaching equilibrium under this condition. After drying for 5 days, 5 - 50% of the water up to 20 mm depth evaporated through the surface. After 13 days of drying, the water content in the first 5 mm in depth reduced very slowly. On the other hand, the water from more than 5 mm in depth moved rapidly.



Figure 3. XZ cross-sectional images for each dry material age for paste, crushed stone, and crushed brick.





Figure 5. Intensity rate based on intensity difference between saturation and equilibrium.

3.3 Measurement Results Using DVC

Figure 6 shows the volumetric strain distribution inside the 3 specimens based on DVC measurement.

In the case of the paste specimen, there was no particular change over the first 8 days drying period. However, the shrinkage strain region can be seen to extend from the side surface after 13 days and extends to about 20 mm depth from the side at 21 days. From 35 to 134 days of drying, the shrinkage strain region widened on the whole. Localised regions of high dilation indicate the formation of cracks.

In the case of the specimens containing the particles of crushed stone and crushed brick, it can be seen that the shrinkage strain increased with drying, as in the case of paste. However, after 35 days of drying, the shrinkage strain around the particles appears to be smaller than in



Figure 6. Volumetric strain distribution inside the specimen based on DVC measurement.

other regions. Several areas of minor dilation can be observed after 8 days of drying which evolve to cracks in the later stages, these appear to form from the particle surfaces early in the drying sequence and then their width increases with further drying. It is likely that the cracks initiated at the particle surfaces due to adhesion between the particles and the paste constraining the shrinkage process.

The results presented above show that the shrinkage strain distribution in the cement paste due to drying from the surface could be measured. In addition, the relaxation of the shrinkage strain was observed around particles, but it was obscured, in part, due to the occurrence of cracks. In future work, specimens that do not crack easily, such as mortar specimens, could avoid this issue.

In addition, the results for the paste specimen in Figures 2 and 3 show that a noticeable shrinkage strain occurred when there was over 50 % difference in the moisture content between saturation and equilibrium. This is considered to indicate that relationships between the internal moisture and volumetric strain can be investigated using X ray CT.

4 Summary

The purpose of this study was to perform length change tests on cylindrical specimens of cement paste using X ray CT as a basic study for measuring drying shrinkage distribution inside concrete and to make measurements using X-ray CT images at different stages of drying. The key conclusions from this work are:

- it was shown that the moisture content inside the paste specimen could be estimated from the intensity changes in the X-ray CT images;
- measurement by DVC analysis of the X-ray CT images showed volumetric shrinkage strain distributions inside the paste specimen and the process of cracking due to the restrictions by the aggregates;
- By integrating the results on image intensity changes and the volumetric strain, it will be possible to clarify the coupling of the local the volume change and the local water content change inside a specimen.
- In this study and the given conditions, a noticeable shrinkage strain occurred when the of the difference of moisture content between saturation and equilibrium was above 50 %.

In summary, this study has demonstrated that internal moisture movement and volume changes due to drying can be considered by image measurements on X-ray CT images, which opens the door to further investigations in the future.

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