

## Influence of Grid Presence in the Characteristics of Applied Mortars

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**Abstract.** *The most commonly used wall coverings are still, undoubtedly, plasters and renders, whether lime-based or cement-based, whether traditional and prepared in-situ or pre-dosed. In accordance with the available standards, the characterization of these mortars is made on laboratory test specimens, with dimensions, curing conditions and test procedures according to the prescribed. However, when applying these mortars to the real substrates, their behaviour will not be the same. After application of the mortar to the substrate, an interface will be formed, and the interactions that occur after the contact of the mortar, still in the plastic state, with the substrate will change over time due to the hydration kinetics and absorption of the substrate. It is very important to know the real behaviour of mortars after application, in order to ensure their durability. A research project is being developed to analyse the proper behaviour of mortars after application to the substrates. In order to characterize a mortar after application to a substrate, it is necessary to detach it. The introduction of a fiberglass grid in the mortar-substrate interface makes the detachment easier. The purpose of this study is to determine if the placement of this grid will influence the characteristics of the applied mortar. For this, an experimental campaign was carried out, comparing the characteristics of two mortar formulations, applied to different types of substrate (without introduction of the fiberglass grid), with the characteristics of these mortars applied to the same substrates, but with the introduction of a fiberglass grid at the interface mortar-substrate. In this paper, we present the results obtained for some of the physical and mechanical characteristics of cement and hydraulic lime mortars.*

**Keywords:** *Mortars, Substrates, Interface, Durability, Fiberglass Grid.*

### 1 Introduction

Mortar based coverings are widely used in all types of constructions, whether new or old, in need of rehabilitation or requalification. When we talk about exterior coverings, we are talking about the outermost layer of protection of these constructions, i.e. the layer that will contribute most strongly to their durability. There is an increasing variety of available solutions, and it is very important to ensure the quality of the applied mortars, since they must contribute to the habitability, comfort and durability of buildings. In recent years, much research has been conducted to increase knowledge on the behaviour of different types of mortars and to develop new formulations incorporating new products, so that one can always make the best choices, regarding the type of mortar to be used, its composition and characteristics.

The choice of the mortar that is best suited to the real situation is based on its various properties, which are determined in laboratory, following all applicable standards, particularly with respect to the dimensions of the test specimens, curing conditions and test methodology.

After the mortar has been selected, it is applied to the real substrate — and there are various

types of substrates, such as hollow brick, solid brick, pre-cast concrete, concrete blocks, natural stone, among others. It is known that inter-layer adhesion is one of the key performance indicators of multi-layer systems. The behaviour of mortars depends on the adhesion between the substrate and the mortar itself. This is one of the characteristics that will influence the properties and behaviour of the mortar (Moropoulou *et al.*, 2000).

When applying a mortar to a real substrate, which will always have some porosity — unlike the laboratory moulds where the specimens that are used to characterize mortars are made, which have virtually no porosity —, an interaction will occur between the two surfaces. The contact between these two elements occurs with the mortar still in the plastic state. When this contact occurs, part of the mixing water, containing dissolved components of the binder, is absorbed by the substrate and penetrates its pores and/or discontinuities. Inside the pores of the substrate, hydration phenomena of cement/lime occur. After this penetration into the substrate and during the subsequent mortar hardening phases, the mortar is subjected to real climatic conditions, which may be quite different from the curing conditions recommended by the mortar characterization standards.

From the foregoing, it can be concluded that the same mortar moulded into specimens and hardened in the laboratory, under standard curing conditions, when applied to real substrates subjected to real climatic conditions, will not acquire equal characteristics. Thus, in order to choose a mortar more rigorously, it is very important to predict the behaviour of the mortar after application to the substrate.

With the objective of being able to estimate the characteristics of the mortars applied to a substrate, using the mortar characteristics determined in laboratory conditions, a research project funded is under development: IF MORTAR.

The aim is to compare, for the same mortar, the characteristics analysed in laboratory specimens with the characteristics determined after application to the substrates. For this, it is necessary to apply the mortars to the substrates and, after hardening, to detach and analyse them. To facilitate the detachment of these mortars, a fiberglass grid has been introduced between the mortar and the substrate. However, a question arises: will the introduction of the grid change the characteristics of the applied mortars? To answer this question, a preliminary experimental campaign was carried out, comparing the characteristics of the mortars applied to the substrates, with and without the application of the grid. Until now only two prescribe mortars were analysed, but the intention is to also analyse design mortars.

## **2 Experimental Campaign**

### **2.1 Introduction**

The experimental campaign developed aimed to analyse the behaviour of cement and hydraulic lime mortars applied to hollow ceramic brick substrates, in two different conditions: with and without the introduction of a fiberglass grid between the mortar and the substrate.

For this, a fiberglass grid was applied to half of the hollow brick substrates. Then, all the brick substrates were moistened and a 1.5 cm mortar layer was applied (Figure 1).

The following mortars were selected for the experimental campaign:

- Cement mortar, with a 1:4 cement to sand ratio, by volume;
- Hydraulic lime mortar, with a 1:3 lime to sand ratio, by volume.

Both mortars were formulated in the laboratory.



**Figure 1.** Application of the mortar to the substrate.

## 2.2 Specimens and Tests

The experimental campaign began with the execution of 40x40x160 mm<sup>3</sup> prismatic specimens, for the determination of the bulk density, open porosity (NP EN 1936:2008), capillary water absorption (ISO 15148:2002) and compressive strength (EN 1015-11:1999), and cylindrical specimens (100 mm diameter and 15 mm thickness) for the determination of water vapour permeability (NP EN 1015-19:2008 and ISO 12572:2016) (Figure 2).

After the detachment of all mortars from the substrates, specimens of appropriate dimensions for the respective tests were cut. Given the thickness of the applied mortars (1.5 cm), it was not possible to obtain specimens with the exact dimensions indicated in the standards. Therefore, instead of 40x40x160 mm<sup>3</sup> specimens, 40x40x15 mm<sup>3</sup> specimens were used for the determination of bulk density, open porosity, capillary water absorption and compressive strength. For the determination of water vapour permeability, cylindrical specimens with 100 mm diameter and 15 mm thickness were used.

After the execution of the laboratory specimens and application of the mortar layer on the substrates, all specimens were subjected to the following standard curing conditions: 20°C and 95% RH, for 7 days, and 20°C and 65% RH, for another 21 days.



**Figure 2.** Test specimens.

The results of the tests carried out are presented and commented in the following section. Even though the main objective is to compare the behaviour of the mortars applied to the substrate, the results obtained for the mortars hardened in the laboratory moulds are also presented.

## 2.3 Presentation and Analysis of Results

### 2.3.1 Bulk density and open porosity

The determination of the bulk density by the geometric method, which translates the simple direct relationship between the dry mass of a specimen and its apparent volume (volume limited by the outer surface of the specimens, including all voids) and the determination of the open porosity, which represents the relationship between the open pores volume and the apparent volume of the specimen, was conducted according to the standard. Figures 3 and 4 show the medium values and standard deviation obtained for bulk density and open porosity, respectively, for the specimens hardened in the moulds and for the specimens hardened on the substrates (with and without grid). It can be seen that the open porosity of the mortars decreased and the bulk density increased, after application to the substrates, as was expected.

When comparing the results of the mortars applied with the grid with those of the mortars applied without grid, it can be seen that they are very similar, i.e. the presence of the grid does not affect the results obtained.

### 2.3.2 Capillary water absorption

The water absorption coefficient gives an indication of the water absorption capacity of a mortar when placed in contact with a water film. The results obtained for the water absorption coefficient, for all the mortars, are presented in Figure 5. Once again, it can be seen that the application of the mortars to the substrate changed this parameter, causing it to decrease. It is also possible to observe that the difference between the results corresponding to the two conditions of application (with and without grid) is small.

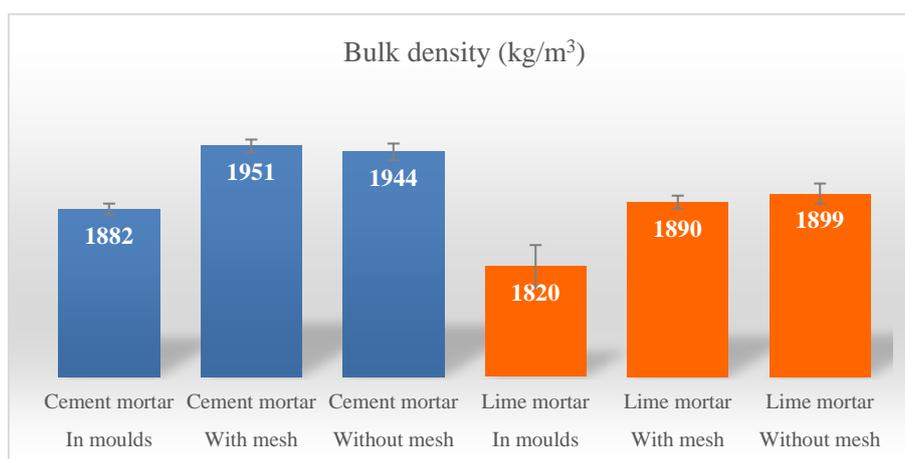
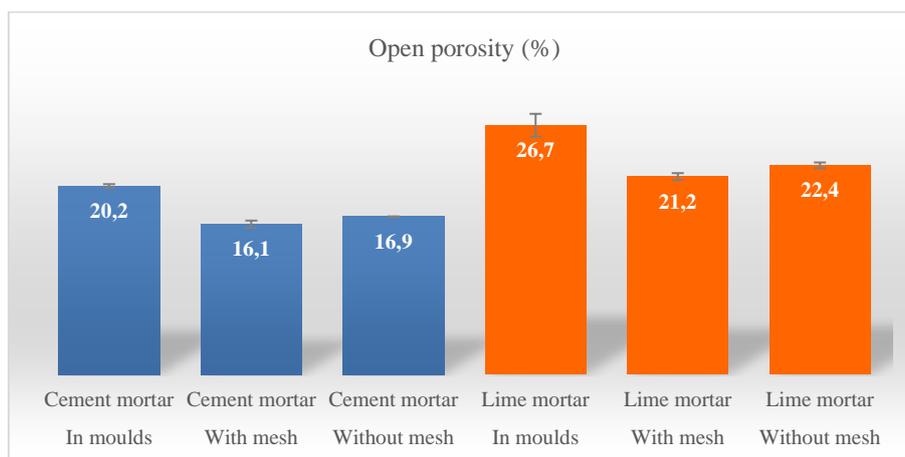
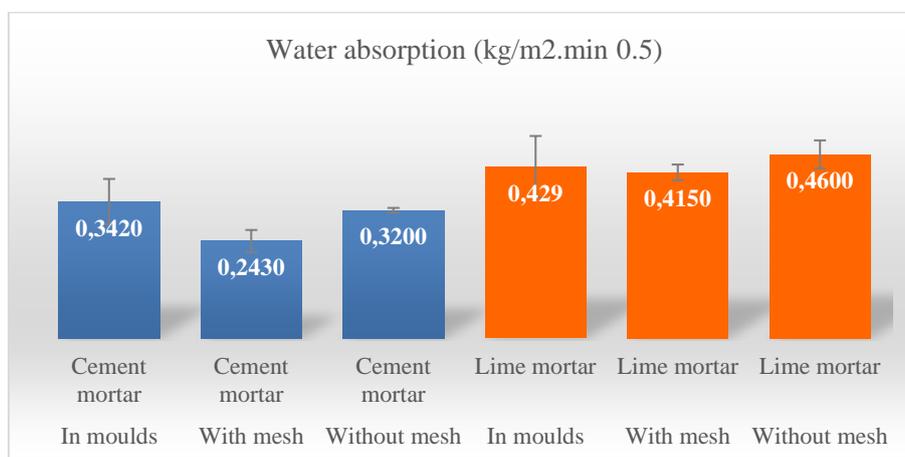


Figure 3. Bulk density.



**Figure 4.** Open porosity.



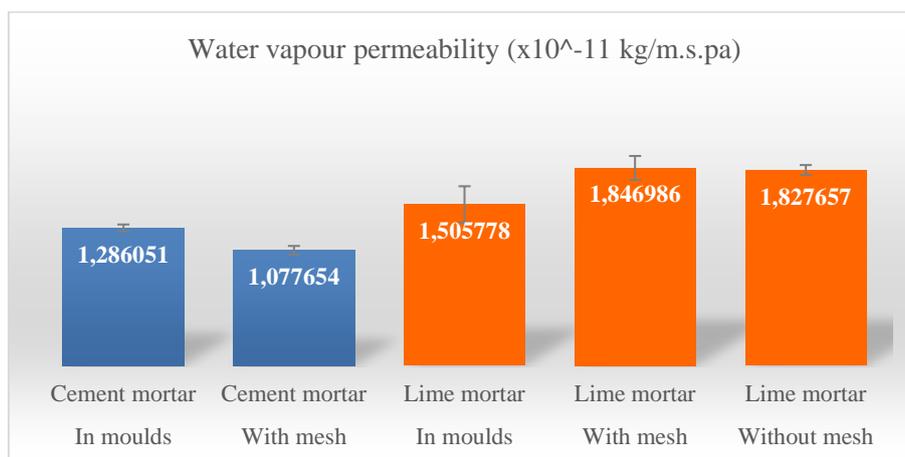
**Figure 5.** Water absorption coefficient.

### 2.3.3 Water vapour permeability

The water vapour permeability coefficient, which reflects the ability of a material to be traversed by water vapour, was determined using the wet cup method.

Figure 6 shows the water vapour permeability coefficient results obtained for all the mortars.

The application of the cement mortar to the substrate led to a decrease in its water vapour permeability, while the application of the hydraulic lime mortar led to an increase of this parameter. In the case of the cement mortar applied to the substrate without grid, it was not possible to detach specimens for this test due to the high cohesion of the mortar to the substrate. For the hydraulic lime mortar, it was verified, once again, that the difference between the results of the detached specimens with and without grid were not significant.

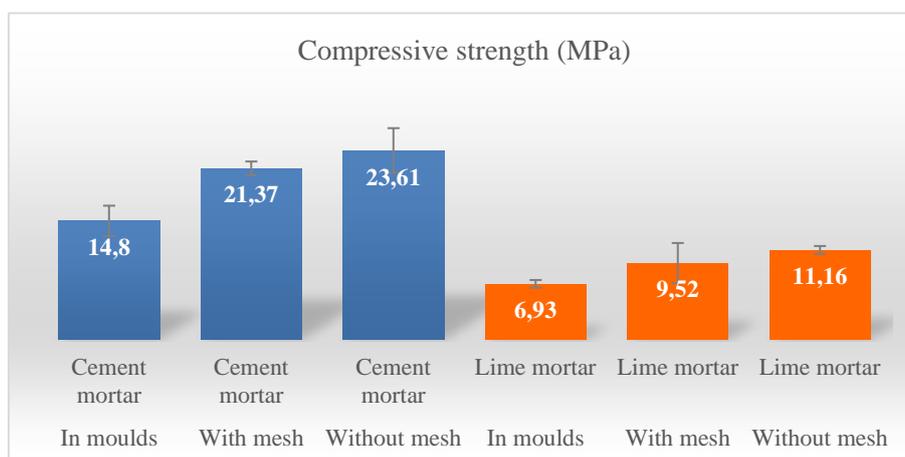


**Figure 6.** Water vapour permeability.

### 2.3.4 Compressive strength

As it is not possible to cut specimens of sufficient size for the flexural test from the mortar layer applied to the substrates, only the results obtained for the compressive strength are presented here. The compressive strength is obtained by applying a compressive force (until failure) centred on the application area of  $40 \times 40 \text{ mm}^2$ .

The compressive strength was determined on specimens measuring  $40 \times 40 \times 15 \text{ mm}^3$ , both for the mortars hardened in the laboratory moulds and for the mortars applied to the substrates. Figure 7 presents the results obtained. It can be seen that the application to the substrates increased this property and that the introduction of the grid does not have great influence on the results.



**Figure 7.** Compressive strength.

## 3 Conclusions

In order to choose a mortar in a more sustained way, regardless of its intended purpose, it is essential to know its behaviour, *i.e.* to know all its properties. These properties are determined

on mortars hardened in moulds, in the laboratory, in accordance with the applicable standards.

The mortar in service, i.e. after application to the substrate, will acquire different properties from those determined in the laboratory, because the application conditions, interface characteristics, curing conditions, etc., are different from those considered in the laboratory.

To have knowledge of the in-service characteristics of mortars, it is necessary to apply them to the substrates, wait for them to harden, detach them from the substrates and, finally, analyse them.

Mortars are applied to the substrate in the plastic state and, when hardened, will adhere to it. The greater their adherence to the substrate, the more difficult their detachment will be. To facilitate this detachment, a grid can be introduced between the substrate and the mortar, but it is important to know whether this grid will affect the final properties of the mortar. The main objective of this work was thus to analyse the influence of the presence of a fiberglass grid, placed between the mortar and the substrate, on the properties of the applied mortars.

The experimental campaign conducted, which included the analysis of the influence of the presence of the fiberglass grid in the behaviour of cement and hydraulic lime mortars, concluded that the properties of the mortars do not change significantly due to the presence of this grid.

In fact, it was observed that the presence of the grid caused a slight increase in open porosity which also slightly increased water absorption and vapour permeability.

Although it was not the main objective of this work, the behaviour of the two mortars moulded in the laboratory moulds was also analysed and compared with the behaviour of the mortars applied to the brick support. Observing the obtained results, it was possible to conclude that the application of the mortars in the support caused the increase of the bulk density and the decrease of the open porosity. The behaviour face to the presence of water was also affected. The water absorption coefficient also decreased. This behaviour is in line with what was expected because when the mortar of the fluid state comes into contact with the brick support, which is a porous material, part of its mixing water with the finer particles dissolved are absorbed and penetrate into its pores. This decrease in the amount of water causes lower porosity with the consequent increase in bulk density and decrease in water absorption.

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