# Application of Passive Drag Reduction Methods to a Generic Strut-Braced Wing





#### Richard L. Campbell Sally A. Viken Michelle N. Lynde

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- Introduction
- Baseline Evaluation
- Approaches to Drag Reduction
  - Aerodynamic Design (CDISC)
  - Passive Porosity (PASSPORT)
  - Comparison of CDISC and PASSPORT Results
- Concluding Remarks

# Introduction







Boeing/NASA 4.5%-Scaled Truss-Braced Wing Model in NASA Ames 11-Foot Transonic Tunnel

### Why Strut-Braced Wings?

- Increasing wing aspect ratio reduces lift-induced drag and can lead to significant fuel savings
- Aspect ratio can be increased to 20 or more if supported by strut or truss
- NASA is investigating strut-braced wing configurations to meet its N+3 goals of reducing fuel burn by 60%

## Introduction





#### **Challenges with Strut-Braced Wings**

- Wing-strut aerodynamic coupling has tendency for shock to develop in juncture region at transonic conditions
- Shock in juncture region increases drag and can lead to separation

# **PADRI Workshop**

#### **Goal of Workshop:**

- Explore candidate flow control technologies and optimization strategies to minimize shock wave and interference drag in wing-strut juncture region
- Apply and evaluate drag reduction strategies to simplified strut-braced wing configuration at transonic conditions

#### **Flight Conditions:**

- Mach = 0.72,  $\alpha$  = 1 deg., altitude = 30,000 ft.
- Adjust angle of attack of configuration with drag reduction mechanism to maintain initial total lift







# **PADRI Workshop Constraints**





### Wing:

- Can only alter between spanwise region of 14.5 m < Y < 17.5 m
- Cannot be modified: upper surface, twist, chord length
- Original lower surface cannot be penetrated

### Strut:

- Can only alter between spanwise region of 14.5 m < Y < 17.5 m
- Cannot be modified: maximum thickness, chord, spanwise wing attachment location, length of vertical portion



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## Unstructured grid generation: VGRID

- Triangulated surface grid, tetrahedral volume cells
- Advanced layers in viscous regions, advancing front in outer flow
- Grid clustering control via line and volume sources

### Navier-Stokes flow solver: USM3D

- Unstructured tetrahedral volume grid
- Cell-centered upwind scheme, no limited used
- Spalart-Allmaras (SA) turbulence model
- Passive or active porous surface boundary conditions available



Grid	Flow Solver	Turbulence Model	<b>Total Elements</b>
Workshop	TAU	SA	59.3 million
VGRID	USM3D	SA	31.0 million



# **Baseline Grid Comparison**





PADRI Workshop

# **Baseline USM3D Solution Convergence**





# **Baseline Solution Comparison:** Pressure



12



# Baseline Solution Comparison: Skin Friction





13

# **Baseline Solution Comparison:** Mach Contour



Y = 15.0 m



NASA



- USM3D and Workshop baseline solutions are generally in good agreement
- Results at Y = 16.5 m show some difference in shock strength and separation extent, not enough information on Workshop solution to assess cause of differences
- Initial studies with USM3D using multiple grids and grid generators showed similar differences with Workshop solution at Y = 16.5 m
- Final grid for design studies chosen based on reasonable size and stronger shock (conservative)



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- Knowledge-based design uses prescribed flow/geometry sensitivity derivatives
- Flow constraints automatically generate target pressure distributions
  from current analysis pressures
- Geometry constraints incorporate multidisciplinary influences
- Modular Linux script approach allows easy coupling of CDISC with a wide range of flow solvers (USM3D, CART3D, MSES, OVERFLOW, CFL3D, PMARK, FUN3D, etc.)
  - Design time ≈ analysis time (1-3 orders of magnitude faster than optimization)
  - Allows use of same level of geometric and flow physics fidelity in design and analysis

## **CDISC Applications for Drag Reduction**

- **Drag Prediction Workshop** • (DPW) W1 Wing
- Gulfstream G650 ٠
- **FAST-MAC** National Transonic ٠ Facility model
- D8 "Double Bubble" •
- **Truss-Braced Wing** ٠
- Lockheed Martin Advanced ٠ Hybrid Wing Body
- **Boeing High Speed Slotted Wing** ۲



20

Aggregate Drag Reduction (counts)

10

Reduced shock -1.2 strength -0.8 -0.4 0 0.4 Baseline Target

 $\mathbf{C}_{\mathbf{P}}$ 

50



30

40



## **CDISC Applications for Laminar Flow**











#### **Flow Constraints:**

- Mach levels limits
  - M<sub>shock</sub> < 1.0 on wing
  - M<sub>shock</sub> < 1.1 on strut
- Modified Uniform Distribution (MUD) to unload strut
- C<sub>P</sub> smoothing

### Geometry Constraints:

- Section (t/c)<sub>max</sub> and leading-edge radius fixed
- Curvature limits, surface and twist smoothing for realistic geometry
- "Hard surface" restriction applied to wing lower surface

$$c_{d,wave} = \frac{0.49}{k} * (M_{shock} - 1)^{4.39}$$

where  ${\bf k}$  is surface curvature, shows that

 $M_{shock}$  < 1.1 produces less than 1 count of wave drag

(AIAA 2011-3527)

# **CDISC Design Station Layout**







# **USM3D Convergence for CDISC Design**





## **CDISC Results:** Wing at Y = 15.0 m





## **CDISC Results:** Wing at Y = 16.5 m





## **CDISC Results:** Strut at Y = 15.0 m





# **CDISC Results:** Strut at Y = 16.5 m





# **CDISC Results:** Mach Contour





# **CDISC Results:** Entropy Contour





# **CDISC Results:** M = 1.1 Shock Isosurface





- CDISC CHANL constraint creates a flat-sided channel between the wing lower surface and the strut upper surface
- Wing lower surface flattened while remaining outside of original airfoil, extent based on amount of supersonic flow
- Strut rotated down slightly, then cambered to make most of upper surface flat
- Lower surface curvature constrained while maintaining original maximum t/c
- No target pressures used, only 1 CDISC cycle required
- → Wing-only, strut-only, and wing-strut cases run, wing-strut case had the most drag reduction







**Baseline** airfoil





Add flattened region





Blend flattened region into rest of lower surface


# **One-Shot Design Process for Wing**



Smooth corners



# **One-Shot Design Process for Strut**



**Baseline** airfoil





Rotate airfoil down to align upper surface ordinate at x/c = 0.05with the ordinate at the upper surface trailing edge





Flatten upper surface ordinates from x/c = 0.05 to the trailing edge while maintaining the baseline thickness distribution



# **One-Shot Design Process for Strut**



Smooth corners



# **USM3D Convergence for CDISC Design**





### **One-Shot Results:** Wing at Y = 15.0 m





### **One-Shot Results:** Wing at Y = 16.5 m





### **One-Shot Results:** Strut at Y = 15.0 m





### **One-Shot Results:** Strut at Y = 16.5 m





### **One-Shot Results:** Mach Contour





### **One-Shot Results:** Entropy Contour





### **One-Shot Results:** M = 1.1 Shock Isosurface







Configuration	CL	C <sub>D</sub>	ΔC	ΔC <sub>D,wing</sub>	ΔC <sub>D,strut</sub>
Baseline	0.427	0.0238	-	-	-
CDISC (wing and strut)	0.426	0.0226	-0.0012	-0.0007	-0.0004
One-Shot (wing)	0.427	0.0234	-0.0004	-0.0006	0.0002
One-Shot (strut)	0.427	0.0228	-0.0010	-0.0006	-0.0003
One-Shot (wing and strut)	0.427	0.0225	-0.0013	-0.0010	-0.0002



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# **Passive Porosity (PASSPORT) Concept**





- Originally developed in the 1980s for shock-boundary layer interaction control
- Applications include shock strength reduction and aerodynamic flow control
- Pressure differences on the outer surface "communicate" through the plenum
- Small amounts of flux through the porous surface alters its effective aerodynamic shape



#### **Porous control effector wind tunnel test**

- NACA 0012 airfoil section
- NASA Langley 8-Foot Transonic Pressure Tunnel
- 1.08% average porosity on full-chord upper surface



# Porous Patch Locations $V = 14.0 \text{ m}_{Y=16.5 \text{ m}}$

- 15% porosity on each patch
- Porous patches extending from Y = 14.5 m to 16.5 m
- Wing lower surface x/c = 0.4 0.5
- Strut upper surface x/c = 0.4 0.6
- Cases run with porous patch on wing-only, strut-only, and wing-strut
- Strut-only case had most drag reduction

### **USM3D Convergence for Porous Case**

















### **Porous Results:** Strut at Y = 15.0 m









### **Porous Results:** Mach Contour





### Porous Results: Entropy Contour





### **Porous Results:** M = 1.1 Shock Isosurface







Configuration	CL	C <sub>D</sub>	ΔC <sub>D</sub>	$\Delta C_{D,wing}$	ΔC <sub>D,strut</sub>
Baseline	0.427	0.0238	-	-	-
Porous (wing)	0.427	0.0237	-0.0001	0.0006	-0.0006
Porous (strut)	0.427	0.0235	-0.0003	-0.0002	-0.0001
Porous (wing and strut)	0.427	0.0237	-0.0001	0.0005	-0.0006



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### Comparison of CDISC and PASSPORT Results

Concluding Remarks

# **Summary of Drag Reduction Approaches**



Configuration	CL	CD	ΔCD
Baseline	0.427	0.0238	-
CDISC (wing and strut)	0.426	0.0226	-0.0012
One-Shot (wing and strut)	0.427	0.0225	-0.0013
Porous (strut)	0.427	0.0235	-0.0003



M = 1.1 Shock Isosurface

# Wave Drag Function on Wing Lower Surface





# **Separation Function on Wing Lower Surface**





# Wave Drag Function on Strut Upper Surface





# **Separation Function on Strut Upper Surface**











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- USM3D and Workshop baseline solutions appeared to be similar, more information needed to assess minor differences
- Both CDISC and One-Shot design approaches were effective at reducing shock strength and flow separation in the design region
- CDISC required about the same time as the baseline analysis, One-Shot required less than a third of that
- The porous cases all had weakened shocks on the component(s) to which porosity was applied, but flow separation occurred from the porous region to the trailing edge, negating the wave drag benefits
- As the above methods are passive, no operational penalty is expected, though manufacturing costs could be increased



- Use the One-Shot case as a starting point for optimization or further refinement with CDISC
- Design entire strut, perhaps including a spanwise loading constraint
- Investigate both passive and active approaches to eliminating the flow separation associated with porosity
- Look at off-design performance, perhaps a multipoint design



Contact: richard.l.campbell@nasa.gov