Deterioration Prediction Model of Multi-Layer Coating Material and its Reference Service Life Evaluation in Terms of Carbonation Control Effect

Kotaro Etchuya¹, Keiichi Imamoto² and Chizuru Kiyohara²

¹Japan Building Coating Materials Association, ecchuya@nsk-web.org

² Tokyo University of Science, Dr.Eng, imamoto@rs.tus.ac.jp

Abstract. In this paper, authors propose a method to predict deterioration of exterior finishes using Markov Chain Model based on field survey results on cracks of exterior finishes of existing RC buildings. There existed correlation between degradation of finishing and carbonation progress. Authors propose the service life prediction approach to focus on the carbonation suppression effect into the concrete considering progress of exterior finish deterioration.

Keywords: Masonry Coating, Visual Survey, Markov Chain Model, Service Life Prediction Method.

1 Introduction

Carbonation of concrete is one of the factors that determines the life of reinforced concrete buildings. In general, it is possible to prevent the carbonation and extend the life by applying an exterior coating material to the outer wall.

It is difficult to predict the degradation of finishing coatings because type of material, parts used, construction level and maintenance level interactively affect the degradation of coating material.

On the other hand, since the exterior finishing coatings is required to have protection performance against reinforced concrete, its end would be evaluated as a time when the carbonation suppression effect decreases a certain value. However, there are many unknown points about the relationship between the deterioration of the exterior coating material and the reduction of the carbonation suppression effect.

In this study, authors investigate the deterioration state of actual buildings throughout field survey, and propose a deterioration prediction method of exterior coating materials by using the Markov chain model, which is one of the comprehensive probabilistic models based on the results of the survey. In addition, focusing on change of carbonation suppression effect with deterioration of the exterior coating material, authors propose a method for evaluating the service life of the coating material.

2 Development of Deterioration Prediction Method for Exterior Coating Material

2.1 Collection of Deterioration Data of Exterior Coating Materials in Real BSuildings

Four reinforced concrete buildings shown in Table1 were surveyed from 2012 to 2016. It should be noted that "Age from Repaint" means the age of the exterior coating material from renovation year to 2016. In addition, since the four buildings locate in the neighborhood, it would be a

close environmental condition. The number of renovations of the exterior coating material is one, but years of the renovation is different.

Table 2. Classification of Crack Degradation.

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		Survey I	Buildings		N ROAD AND	The state of the s	(range 50mm×50mm)
	A	В	С	D	为你们在这次是	at the second	(runge somm somm)
Construction	reinforced concrete construction				12 AS 6 12 A	the state of the state	Grade O :
Stories	4	4	4	12	6. 18. 6. 9. 9. 8. 8	Carried and the	No crack
Design Strength	18 N/mm ²	18 N/mm ²	21 N/mm ²	21 N/mm ²			Grade I :
Year of construction	1978	1977	1977	1977	Grade O	Grade I	A few cracks
Year of Repaint	2010	2008	2001	1997			Crada II.
Age from Repaint	6 old	8 old	15 old	19 old	and the second	Car and Ar	Grade II .
Coating Material	Multi-layer Coating Material (E Type)				NE ALLA	C. F. S. S.	About 10 cracks
(construction)							Grade III :
Coating Material (repaint)	Synthetic Resin Emulsion Paint				N. F. S.		Mesh type cracks overall
Color of finish	white						
					Grade II	Grade III	

 Table 1. Surveyed Buildings.

Survey items are as follows.

- (1) Cracks: Visual cracks in the outer wall were classified into four grades. About 100 to 200 points with each point of 50mm x 50mm area for each building were surveyed. Grade detection was performed using a standard sample shown in Table 2.
- (2) Carbonation: Carbonation depth was measured by phenolphthalein solution method with core specimens.

Fig. 1 shows relationship between elapsed years after the repair of the surveyed buildings and average crack grade of each surveyed location. As an overall trend, it was confirmed that cracking progressed with the passage of time since the renovation.

Fig. 2 shows relationship between elapsed years since renovation and depth of carbonation. It can be seen that the progress of carbonation is delayed as the passage of time from the renovation increases. Since age of each surveyed building is almost the same and the number of repaints is one, it would be thought that not only the aging from the renovation to the time of the survey, but also the aging from the new construction to the renovation affected the progress of carbonation. Furthermore, the carbonation progressed in the buildings where the renovation time was significantly delayed.



Figure 1. Crack Degradation.

Figure 2. Carbonation.

2.2 Deterioration Prediction of Exterior Coating Materials

The Markov chain model is a probabilistic model for future condition prediction, and it is a

macro model that is used when it is difficult to predict by the accumulation of each affecting factor. Here, in the degradation grades from O to III as shown in Fig.3, the transition probability Xn is assumed to transit from certain degradation grade to the next grade after a certain time t. It is assumed that the distribution of the deterioration grade at any time can be simulated. This model has irreversible features, and its equation is represented in Fig.4.

As shown in Fig. 1, cracking phenomenon, which is the degradation phenomenon of exterior coating, tends to progress with time, and is consistent with the irreversible characteristics of the Markov chain model used in this study.



Average values of the transition probability based on the results of the crack survey from 2012 to 2016 are shown in Table3. In addition, the results of prediction of deterioration of cracks by Markov chain model using the transition probability are shown in Fig.5.

Feature of this model is as follows. At the time of "0 years", crack grade 0 occupies the entire building, but the proportion of crack grade I increases as the age progresses, and the crack grade 0 decreases accordingly. Furthermore, the proportion of crack grade II increases as years progress, and crack grade 0 and I decrease. In the end, the ratio of crack grade III, which is the most significant degradation, increases.



Figure 5. Prediction of Cracking.

3 Relationship between Cracking and Carbonation Suppression Effect

3.1 Decrease in Carbonation Suppression Effect by Cracking

Authors examine relationship between cracking and carbonation suppression effect.

Akio, T. (2013) showed that there is a certain correlation between surface air permeability coefficient and carbonation rate coefficient of existing RC buildings. In this study, time change of carbonation suppression effect of a multi-layer coating coating material was evaluated by the

air permeability test. Crack of the coating material is degradation phenomenon as shown in table 2 and CO_2 induced carbonation would occur at the cracks which strongly affects air permeability of the coating. Hence, the deterioration of the coating material and its relation to carbonation would be evaluated with surface air permeability.

3.2 Verification at Laboratory

Multi-layer coating materials for exterior finishing used in reinforced concrete buildings often composed of three layers that are a top coating layer that protects the outer wall from solar radiation and rain, a main material layer that provides texture and a primer layer that improves adhesion to the frame. Here, in order to confirm the possibility that the protective effect of the coating material would be reduced by cracking of the top coating material, the change of air permeability of the surface layer was measured at laboratory.

An outline of test specimen is shown in Fig.6. First, sewing thread is laid down at different intervals on calcium plate. Next, an acrylic resin emulsion paint as an overcoat layer for the exterior coating material was applied to the calcium plate with a roller. After 60 minutes, the sewing thread was pulled out to reproduce pseudo crack.

Surface permeability was evaluated using a double chamber method (1992) before the sewing machine was laid down.

Fig. 7 shows the ratios of the air permeability coefficient of the test specimen before and after crack initiation.

Here, "crack length" represents the total length of pseudo cracks in the range of the chamber of the measuring apparatus.

It can be seen that the air permeability coefficient increases with the increase of the length of the pseudo crack, and finally the air permeability coefficient approached to that of the calcium carbonate plate before coating.

This might indicate that when the cracks in the top coat layer increase, the air permeation becomes easier and the carbonation suppressing effect decreases. And the close air permeability to the substrate calcium carbonate plate at significant crack state might be same as no overcoat layer applied.



Figure 6. Test Models.



Figure 7. Relation of cracking and Coefficient of Air Permeability.

3.3 Survey of Actual Buildings

Crack and air permeability of actual buildings were surveyed. Nine reinforced concrete buildings estates shown in Table4 were surveyed at a position of about 1.5m height above the ground and a visual inspection of the cracks and surface air permeability tests were conducted

at the same location. As a feature of these buildings, each building is under almost same environmental conditions and age of construction and types of coating materials are same.

Fig. 8 shows secular change of crack grade and surface air permeability. As the years progress, the crack grade and air permeability coefficient tend to increase. As a result, there was a possibility that there was a temporary correlation between the cracks and air permeability of the coating material.

Buildings	Building Age	Finishing Material
A	11, 14, 18	Sprayed Tile
В	13, 16, 18	Multi-layer Finish Material
		(Thick E Type Treated Protrusion)
С	7, 9, 11	Sprayed Tile Thick E Type



3.4 Verification Using a Markov Chain Model for Deterioration Prediction Simulation

Kei.M (2013) evaluated period when carbonation rate coefficient of finished concrete became equal to that of exposed concrete due to deterioration of the coating film as the service life of the coating material. It was 13 years according to his study. Here, based on the fact that cracking of the coating material progresses with time in Fig. 1 and that carbonation tends to progress according to time from new construction to renovation, a damage of coating material was assumed to be critical. Hence, "Accumulation of degradation" was set in consideration of the relationship between years that exceeded the limit years and the degree of limit excess of deterioration as shown in the following equation (2). And the relationship between "Accumulation of degradation" and carbonation depth (Kotaro.E(2016)) was examined. Fig. 9 shows a conceptual diagram.

$$D_{a} = \sum_{n=1}^{N} \sum_{t=1}^{T(n)-L} \left(d_{n} \left(L + t \right) - d_{n} \left(L \right) \right)$$
(2)

Here,

Da: Accumulation of degradation", N(times): Number of paintings including when building exterior coating materials, T(n)(year): Number of years from the time of painting to the time of renovation (when n = N, from the time of painting to the time of survey), L(year): Marginal years for exterior coating materials, dn(x): Represents the ratio of degradation grade III (0 <dn (x) <1) of Markov simulation at the time of n times of coating n times, and is considered only when the age exceeds the limit years (x> L).

Based on previous research (2011), the relationship between "Accumulation of degradation" and the mean of the carbonation depth of each building assuming the limit of 13 years is shown in Fig.10 for the surveyed building shown in Table1. It can be seen that the average of the carbonation depth of the building increases as "Accumulation of degradation" increases, and there is a possibility that there is a certain relationship between the crack and the carbonation suppression effect.

Table 5 shows list of the all surveyed buildings. Although these buildings are different specification and subjected to different environmental conditions, design standard strength was close to each other. Hence, "(1) Crack" and "(2) Carbonation depth" using the methods described in chapter 2 were investigated. Fig. 11 shows relationship between "Accumulation of degradation" and carbonation depth for each survey target. Although the correlation of Fig.11 was lower than that of Fig. 10, a certain degree of correlation was kept. Thus, there would be correlation between the cracking and carbonation inhibitory effect of the multi-layer coating material.



Figure 9. Models of Accumulation of degradation.

Α

В

С

D

E

F

G

Н

T

Κ

Τ.

196

Table 5. Survey Buildings



Figure 10. Relation of Accumulation of degradation and Carbonation depth.



4 A proposal for Service Life

In Fig. 10, it would be clear that carbonation depth would be 0, if "Accumulation of degradation" is 0. That means that the regression line should pass through the origin. At this that the regression line passed a bit other point of the figure because the limit age of the coating materials was assumed to be 13 years. Therefore, authors set the new limit years so that the regression line approaches the origin. In the subject of this survey, the regression straight line passed the origin when the limit age was 10 years. Fig. 12 shows the relationship between "Accumulation of degradation" and the carbonation depth with the critical age of 10 years. When the limit service life is assumed to be 10 years, the deterioration rate shown in Fig. 5 (the

ratio of deterioration grade III) would be 16.0% with transition probabilities shown in Table 3. It would be possible to consider the time when this deterioration rate is reached based on carbonation of concrete.

As described above, the exterior coating materials can be used to minimize or control the carbonation of concrete by repainting within a range that does not cause "Accumulation of degradation" within 10 years. In this sense, it can be situated as a way of service life consideration.

The relationship between age and "Accumulation of degradation" is shown in Fig. 13 by Equation (2) for the survey target in Table 1.

In addition, the relationship between age and carbonation depth is shown in Fig. 14 by using the approximate expression of the relationship between "Accumulation of degradation" when the limit years as 10 years. On the other hands, if the cover thickness of reinforced concrete is 30 mm, this building will face to the end of life in 36 years unless it is repainted. Here, assuming that the required service life of the building is 100 years and the repainting interval at which carbonation does not reach 30 mm within 100 years, life cycle assessment of finishing coating in terms of carbonation would be possible. Table6 shows the prediction of the carbonation depth of buildings when the exterior coating materials are refurbished and the age reaches 100 years. It would be calculated that if the exterior coating material used in this building is repainted every 22 years (Fig.15), carbonation does not reach the reinforcing bars within 100 years.



of Carbonation Depth in 100 years.

of Carbonation Depth in 100 years.							
Repaint interval (year)	Prediction of Carbonation (mm)	Repaint interval (year)	Prediction of Carbonation (mm)				
30	55. 21	25	41.80	lati			
29	50.60	24	36. 33	þ			
28	47.11	23	31.19] වි			
27	44. 75	22	26.69				
26	43. 49	21	24. 05				



The findings obtained in this study are shown below.



Figure 15. Prediction of Carbonation depth. (repaint interval 22years and 23years)

- Authors investigated four buildings that were close environmental condition, focusing on cracking of multi-layer coating. As an overall trend, Cracking was confirmed that cracking progressed with the passage of time since the renovation.

- Based on the survey results on cracks in multi-layer coating materials applied to reinforced concrete buildings, authors presented a method for predicting crack degradation using a Markov chain model.

- Authors showed a possibility that there was a correlation between the cracks and air permeability of the coating materials by laboratory experiments and surveys of real buildings. In addition, by considering along with the report that there was a correlation between surface air permeability and carbonation rate coefficient of existing RC buildings, authors showed a possibility that there was a correlation between the cracking and carbonation inhibitory effect of the multi-layer coating materials.

- Authors proposed "Accumulation of degradation" considering the time and grade when the crack exceeded a certain value. And Authors confirmed that there is a certain correlation between the "Accumulation of degradation" and the carbonation depth of the buildings.

- By using the relationship between "Accumulation of degradation" and the carbonation depth of the buildings, Authors suggested the service life for the coating materials to use the buildings for the longest years and the required years.

ORCID

Kotaro Etchuya: https://orcid.org/0000-0002-7858-9420 Kei-ichi Imamoto: https://orcid.org/0000-0001-8174-8827 Chizuru Kiyohara: https://orcid.org/0000-0003-1286-9056

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